REMOVAL OF SOME NEW DIRECT SULPHO ARYL AZO DYES FROM AQUEOUS SOLUTIONS BY ADSORPTION ONTO DIFFERENT TYPES OF CARBON

إزالة بعض صبغات السلفو أريل أزو المباشره الجديده من المحاليل المانيه بالإمتزاز على انواع الكربون المختلفه

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الملخص العربي

تم تحضير مجموعة جديدة من اصباغ اريل آزو المباشرة والتي تعتمد على نواة سبيرو ٢-أكسو اندول (٢،٣) - ٢،١٠ ثيازول وتقييم إمكانية إستخدام تكنولوجيا الإمتزاز للتخلص من الوانها المتبقية في اوساطها المانية. وقد تم اختيار خمسه اصباغ (تمثل المجموعات المختلفة من اصباغ آريل آزو التي تم تحضيرها) لدراسة كفاءة تطبيق طريقة الإمتزاز على أنواع مختلفة من الكربون للتخلص من متبقيات هذه الأصباغ في محاليلها المانية بعد عملية الصباغة واتحقيق ذلك تم اختيار ثلاثة أنواع من الكربون لوسط الامتزاز وهي الكربون المنشط الناعم والكربون المحبب والسناج الناتج من مصنع سماد طلخا ولقد تم تعيين الزمن اللازم للوصول إلى نقطة الإتزان في عملية الامتزاز على أنواع الكربون الثلاثة المستخدمة كوسط امتزاز وذلك عند أربع درجات حرارة مختلفة هي ٢٠، ٥٠، ٢٠ درجة منوية وتم تطبيق معادلات لانجمير وفريندلش وبارنر ايمت وتيلر ووجد ان النتائج متوافقه مع تطبيق هذه المعادلات.

ABSTRACT

A new group of direct arylazo dyestuffs that are based on the spiro 2-oxoindole (3,2')-1',3'-thiazolone moiety was successfully synthesized by the authors [1]. In view of the current interest in utilizing the sulpho arylazo dyestuffs for dyeing different types of fibers, the present paper describes the possibility of using carbon for their removal, as organic pollutants, from aqueous solutions. The removal of these dyestuffs from their aqueous solutions was carried out by using different adsorbents such as granular carbon, carbon soot, and powdered activated carbon (PAC) at different temperatures ranging from 25 °C to 60 °C. The adsorption of these dyes on different types of carbon has been found to obey the adsorption isotherms like Langmuir, Freundlich and Branuer Emmitte and Teller (BET) isotherms. It was found that PAC has the highest capacity of adsorption .Carbon soot is recommended to be used for the removal of such type of dyes from their aqueous solutions due to the low cost of its production with respect to PAC and to solve the problem of its accumulation, as a polluting solid waste. Different adsorption parameters were calculated from these models for the interpretation of the adsorption process. It was found that the removal efficiency for color of dyes was over 90 % in case of carbon soot and PAC at higher temperatures.

KEY WORDS: Adsorption, Langmuir, Freundlisch and Burnaur Emmette & Teller (BET) isotherms, sulpho arylazo dyestuffs.

1. INTRODUCTION

In Egypt the problem of color removal from textile wastewater has considered to be of great importance because of the need to satisfy the increasing demand for water for various uses. For this reason, a national effort has been launched to deal with this problem using natural, local adsorbents. Investigations have been undertaken to determine whether cheap commercially available materials hold promise in the treatment of wastewater. In spite of the presence of a huge number of dyestuffs which are widely used in dyeing processes, little data are available about their removal from dyeing wastewater.

Adsorption is used in industrial wastewater treatment to remove organic materials such as color, phenols, detergents, and other toxic or non biodegradable. The most important component of the cost of using PAC is the cost of PAC itself; therefore, searching for inexpensive sources or substitutes for PAC is a must. Asfour et al. [2, 3] studied the adsorption of basic dyes on hardwood sawdust. Ahmed et al. [4], Sen [5], Gupta et al. [6] and Banerjee et al. [7] used coal fly ash which is a solid waste of thermal power plants as adsorbent. EL-Gundi [8, 9, 10] studied the adsorption of two basic dyestuffs (Astrazone-blue and Maxilon-red), two acid dyestuffs (Telonblue and Erionyl- red), Basic Blue 69 (BB 69) and Basic Red 22 (BR 22) onto maize cobe (an agricultural solid waste). Mckay et al.[11,12] studied the adsorption of four dyestuffs onto bagasse pith (by-product of the sugar industry remaining after the extraction of juice), for the adsorption of two basic dyes(basic-blue 69 and basic-red 22) and two acid dyes (acid-blue 25 and acid-red 114). El-Saiid et al.[13] used the Egyptian bagasse (a waste by-product of

the sugar industry) as adsorbent for the removal of basic dyes namely Rosaniline and Methylene Blue from industrial wastewater. Rashed et al. [14, 15] reported that carbon soot is a promising material for different industrial applications as substitute for commercial powdered activated carbon. Sarkar et al. [16] studied the adsorption of Methyl Violet (C.I. Basic Violet) from aqueous solutions onto coal and fly ash. Al-Sarawy [17] studied the using of carbon soot and PAC as good adsorbents for the removal of colors of some dyes from their aqueous solutions. Safarik et al. [18] used the magnetic charcoal to adsorb a variety of organic compounds. Sankar et al. [19] studied the removal of diazo and triphenylmethane dyes from aqueous solutions using Rice Bran-based Activated Carbon, Ruey-Shin et al. [20] and Feng-Chin et al. [21] used chitosan for removing chlorotriazine reactive dyes and reactive dyes (RR222, RY 145, and RB222) from aqueous solutions. Attia [22] used soot and PAC as adsorbents for the removal of some heavy metals from water. Cheung et al. [23] studied the removal of cadmium ions from effluents using bone charcoal. Shawwa et al. [24] studied the removal of color and chlorinated organics from pulp mills wastewater using activated petroleum coke.

2. MATERIALS AND METHODS

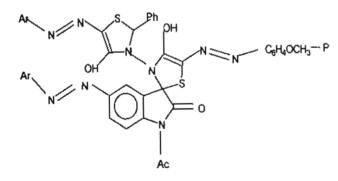
All chemicals and solvents used in this research were of the highest grade of purity. Sodium salts of five dyes of the hitherto synthesized dyestuffs and considered as arylazo spiro thiazolo isatin dyestuffs; their chemical structure is shown in Figure 1 which were previously synthesized by the authors [1]were chosen for studying their adsorption behavior on different types of

carbon at different temperatures. PAC and granulated carbon were obtained from El-Nasr pharmaceutical chemical company. Carbon soot was produced as a result of partial oxidation of natural gas at SEMADCO. Procedures were carried out to study the adsorption of these dyestuffs from their aqueous solutions by using a shaker

with water bath controlling temperature [1]. The remaining dye concentration was measured using a spectrophotometer (Qualen kamp visi-spec SPR-590-010-W). The separation of absorbents from solutions was performed by centrifuge using a bench top centrifuge model T-54.

Dye 1 (Orange, 529 nm)

Dye 2 (Dark red, 541 nm)



Dye 3 (Red, 548 nm)

Ph N N N N Ph

Dye 4 (Blue, 610 nm)

Dye 5 (Dark blue, 613 nm)

Ar 4-sulphophenyl

Fig. 1. Chemical structure of the five direct arylazo dyestuffs.

3. RESULTS AND DISCUSSION

3.1. Effect of Temperature and Retention Time on Adsorption

The results shown in figures (2-6) indicate that the remaining concentration of the five dves in their aqueous solutions decreases with increasing time till equilibrium time is attained and the remaining concentration becomes constant after a time specific for each Results dye. indicate that. equilibrium times for the five dves on different adsorbents different at temperatures were in the range 50-100 minutes. It was found that the suitable doses of adsorbents were; 0.1 mg (soot), 0.5mg (granular carbon) and 0.05 mg (PAC) /10 ml of dye solution . The effect of temperature (25 °C, 40 °C, 50 °C and 60 °C) is clear from these figures since the equilibrium time decreases with increasing temperature due to the fact that by increasing temperature the rate of adsorption increases and equilibrium time decreases [7] .Generally, it was found that, equilibrium time for the adsorption of these dyes on different types of carbon varies significantly for the five dyes and depends only on temperature and is specific for each dye, adsorbate and adsorbent. Also it was found that the removal efficiency for color of dyes was a very good efficiency (over 90 % in case of carbon soot and PAC at higher temperatures).

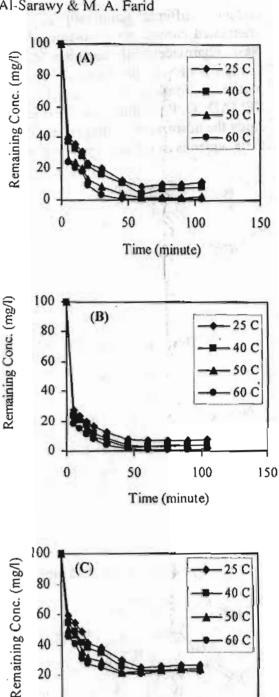


Fig. 2. Effect of time for the adsorption of dye (1): (A) soot, (B) PAC and (C) granular carbon at different temperatures.

50

40

20

0

0

60 C

150

100

Time (minute)

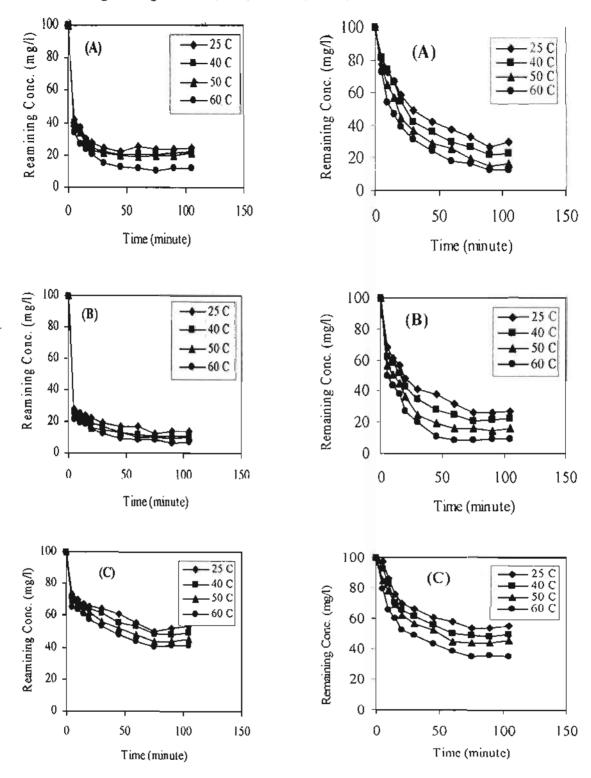


Fig. 3. Effect of time for the adsorption of dye (2): (A) soot, (B) PAC and (C) granular carbon at different temperatures.

Fig. 4. Effect of time for the adsorption of dye (3): (A) soot, (B) PAC and (C) granular carbon at different temperatures.

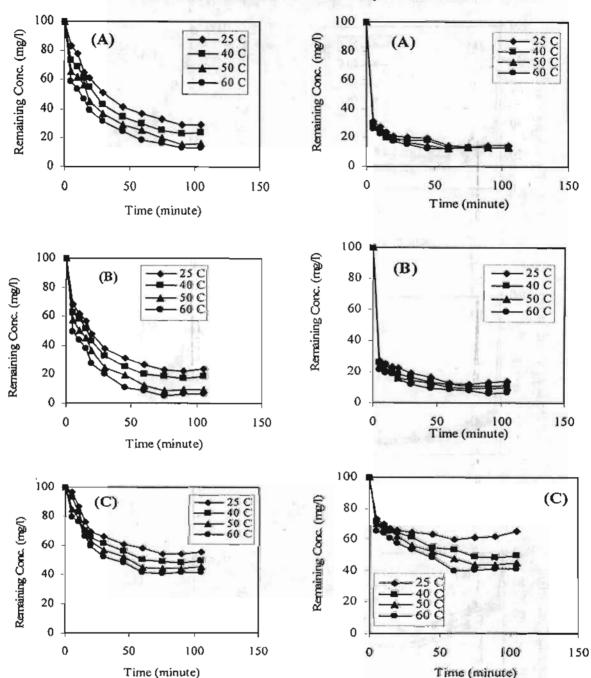


Fig. 5. Effect of time for the adsorption of dye (4): (A) soot, (B) PAC and (C) granular carbon at different temperatures.

Fig. 6. Effect of time for the adsorption of dye (5): (A) soot, (B) PAC and (C) granular carbon at different temperatures.

3.2. Adsorption Isotherms

Analysis of equilibrium data for the adsorption of the dyes on the three types of carbon have been done according to

Langmuir, [25], Freundlich, [26] and Burnauer, Emmett, and Teller [27] models. All adsorption studies were carried out at four different temperatures (25°C, 40°C, 50°C and 60°C).

3.2.1. Langmuir Isotherm

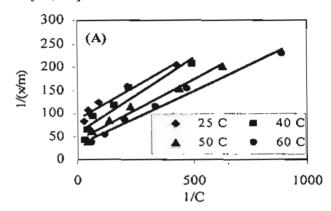
The plots of the reciprocal of the amount of adsorbed dye x/m (mg dye / mg carbon) against the reciprocal of equilibrium concentration (1/C) for the studied dyes gave straight lines as shown in figures (7-11). This indicates that the adsorption process conforms to the Langmuir adsorption isotherm and Langmuir equation is applicable [25]:

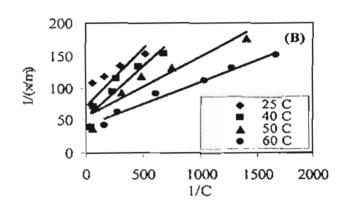
$$x/m = abC/(1 + aC)$$
 (1)

The slope of the best fit (1/ab) and the intercept (1/b) of linear plots Langmuir isotherm for the five dyes were obtained and Langmuir parameters (a) and (b) for adsorption of the dyes on soot, granular carbon and PAC are calculated at the previously mentioned temperatures and listed in table (1). From these results, it was found that (b) values (the indication of monolayer coverage) for PAC > carbon soot > granulated carbon. This is in agreement with the finding in literatures concerning the increase in (b) value with the decrease in the particle size of adsorbent [13, 17, 22]. The monolayer coverage parameter (b) generally increases with increasing temperature.

It was found from electron micrographs that, the particle size of granular carbon > of soot > PAC [28]. This is appeared indicate that the surface area associated with pores inside the particle is being at least partially occupied by the large dye molecules, and that the effective regime is confined to the external surface and a narrow layer just below the surface in the case of PAC [17, 29, 30], whereas in the case of carbon soot the effective adsorption regime is confined in a less extent to the external surface and to the formation of thick layers below the surface. Table (1) contains the equilibrium parameter (R₁) which is defined from the relation [17, 29, 30]:

RL = 1/[1 + a Co] (2) The values of R_L for the studied systems were found to be < 1 showing a favorable adsorption for the tested dyes on carbon soot, granular carbon and PAC [17, 31].





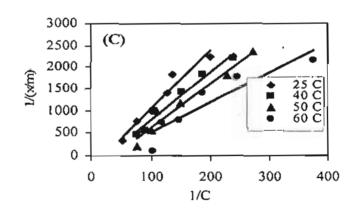


Fig. 7: Plot of Langmuir equation for the adsorption of dye (1): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

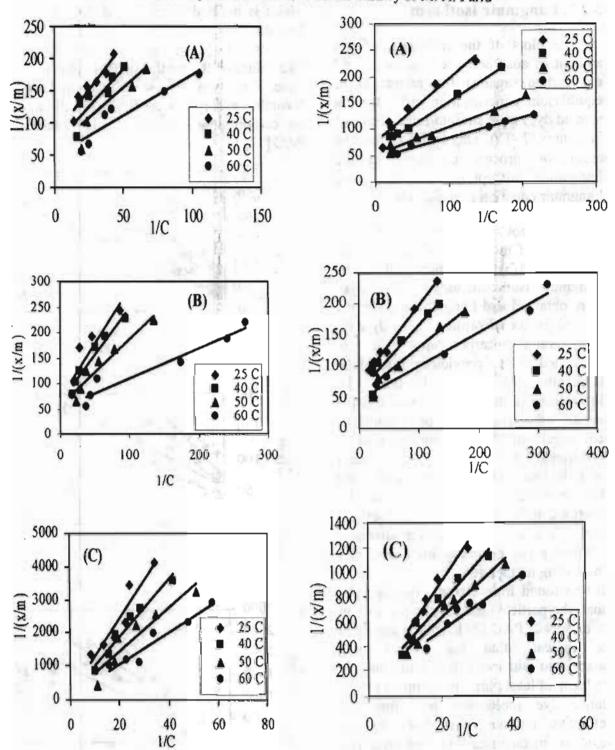


Fig. 8: Plot of Langmuir equation for the adsorption of dye (2):(A) soot,(B) PAC, and (C) granular carbon at different temperatures.

Fig. 9: Plot of Langmuir equation for the adsorption of dye (3): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

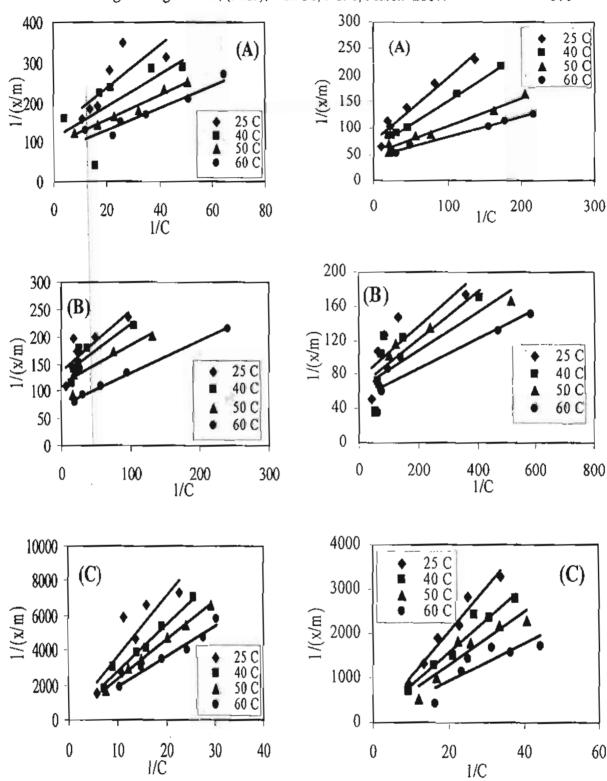


Fig.10: Plot of Langmuir equation for the adsorption of dye (4): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

Fig. 11: Plot of Langmuir equation for the adsorption of dye (5): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

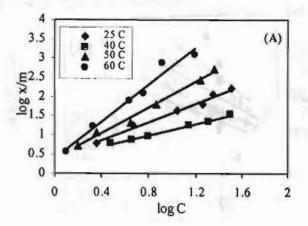
3.2.2: Freundlich Isotherm

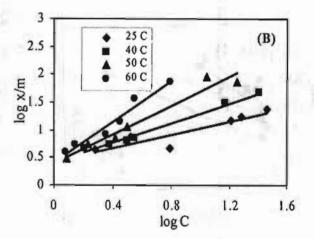
Test of validity of Freundlich adsorption isotherm for adsorption process was followed according to the equation [26, 31]:

$$Log(x/m) = log k + (1/n) log C$$
 (3)

Plotting log (x/m) against log C gave rise to a group of straight lines, Figures. (12-16) corresponding to adsorption of the tested dyes on different types of carbon at different temperatures.

From slope and intercept (1/n) and K (adsorption capacity) values were calculated respectively and delineated in table (2). The delineated data reveals that adsorption capacity values (K) increase as the pore size of carbon change from PAC to carbon soot and finally to granular carbon. This might be explained in view of freundlich equation [17, 26], which implies the two important parameters (K) and (1/n) which are related to the capacity of adsorbent for the adsorbate and the adsorption strength of process respectively. It was found that (n) values are in the range that indicates a good adsorption since (n) values are higher than unity [17, 26]. Moreover these data revealed that direct dependence of adsorption capacity on temperatures. Generally the capacity of the three used types of carbon for adsorption of the chosen dyes could be arranged in the order of PAC >carbon soot >granular carbon.





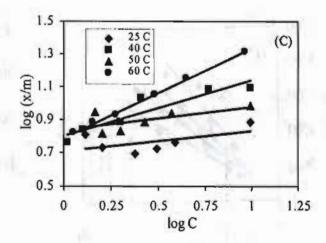


Fig. 12: Plot of Freundlich equation for the adsorption of dye (1): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

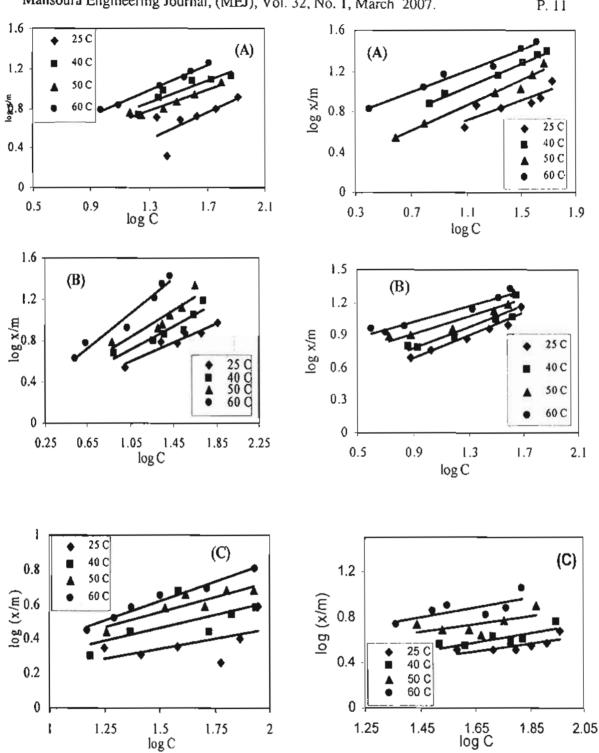


Fig.13: Plot of Freundlich equation for the adsorption of dye (2): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

Fig.14: Plot of Freundlich equation for the adsorption of dye (3): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

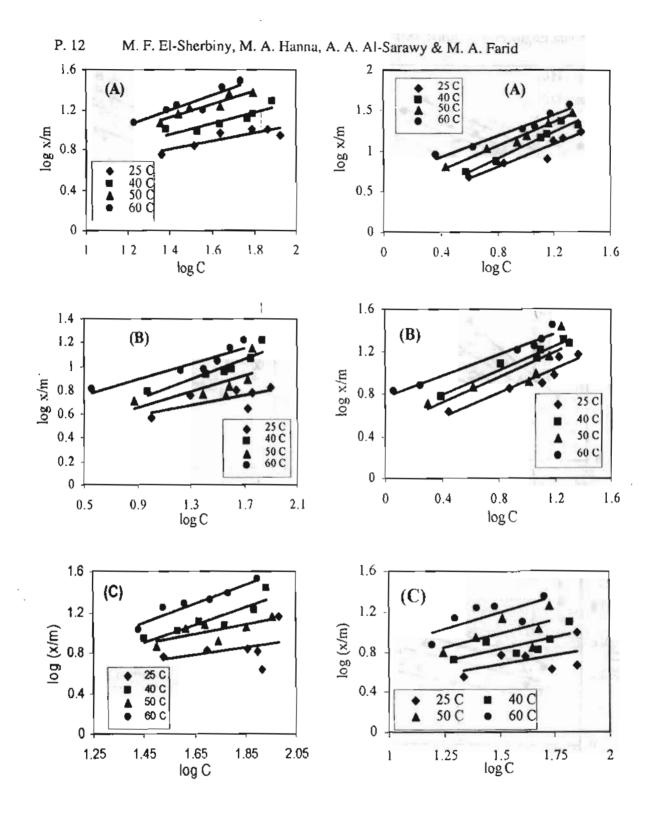


Fig.15: Plot of Freundlich equation for the adsorption of dye (4): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

Fig.16: Plot of Freundlich equation for the adsorption of dye (5): (A) soot, (B) PAC and (C) granular carbon at different temperatures

3.2.3: BET Isotherm

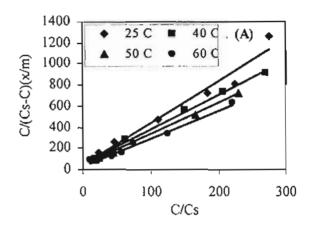
Brunauer, Emmett and Teller [27] derived an adsorption isotherm based on the assumption that molecules could be adsorbed in more than one layer thick on the surface of the adsorbent. This equation, like Langmuir assumes that the adsorbent surface is composed of uniform, localized sites and that the adsorption at one site does not affect adsorption at neighboring sites. Moreover, it was assumed that the energy of adsorption holds the first monolayer but that the condensation energy of the adsorbate is responsible for adsorption of successive layer. The equation, known as BET equation, is commonly written as follows [17, 27]: x/m = ACXm/(Cs-C)[1+(A-1)C/Cs]Rearranging the BET equation yields:

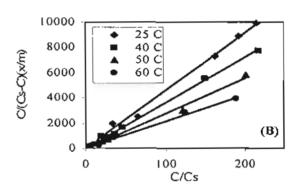
$$\frac{C}{(Cs-C)X/m} = \frac{1}{AXm} + \frac{A-1}{AXm}(\frac{C}{Cs})$$
 (5)

Data obtained from adsorption processes, for the tested dyes on different types of carbon are utilized to conform the BET equation when plotting C/(Cs-C)(x/m) against C/Cs. Figures (17-21) illustrate the resulting straight lines obtained from the BET equation of the tested dyes on different types of carbon, the slope of these lines equal to $A - (1/AX_m)$ and intercept equal to 1/AX_m. Values of both (A) and (Xm) for the tested dyes on carbon soot, granular carbon and PAC are given in table 3.

It's evident that the amount of solute adsorbed utilized in forming a complete monolayer on PAC > carbon soot > granular carbon. The effect of temperature is clearly obvious, hence the value of Xm increase as the temperature increasing from 25 °C to 60 °C. This may be explained on the basis that, the increasing temperature increases the rate of adsorption, moreover, increase the

temperature increases the mobility of the large dye ions for further penetration[9, 17, 27] consequently the adsorption process becomes more favorable with increasing temperature.





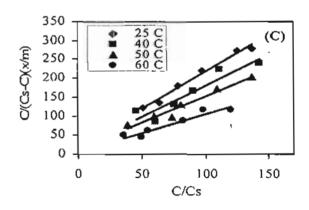


Fig.17: Plot of BET equation for the adsorption of dye (1): (A) soot,(B) PAC, and (C) granular carbon at different temperatures.

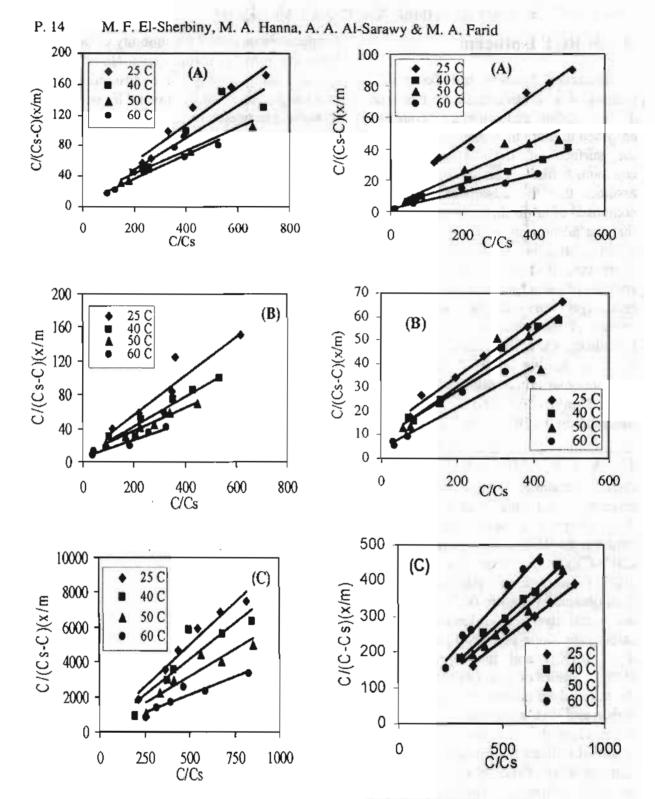


Fig. 18: Plot of BET equation for the adsorption of dye (2): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

Fig. 19: Plot of BET equation for the adsorption of dye (3): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

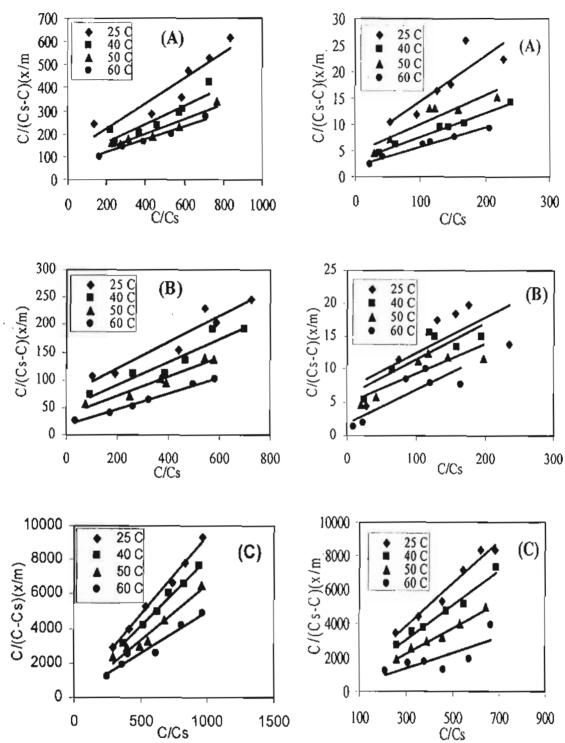


Fig. 20: Plot of BET equation for the adsorption of dye (4): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

Fig. 21: Plot of BET equation for the adsorption of dye (5): (A) soot, (B) PAC, and (C) granular carbon at different temperatures.

4. CONCLUSIONS

This paper studied aims to identify the ability of soot produced as a byproduct from the partial oxidation of a natural gas as adsorbent material (for some of newly synthesized dyestuffs) against conventional carbon adsorbents (PAC and granular carbon). The study reveals that:

Carbon soot is a good adsorbent for removal of these prepared dyestuff from their aqueous solutions at 60 °C, the color of dye is reduced with a very good efficiency over 90 % as shown in figures (2-6).

The data of all parameters obtained in the adsorption study are explained through several adsorption models, all the calculated parameters were found to be in agreement with the finding in literature as indicated from the following:

- Fitting the Longmuir model to the experimental data at different temperatures suggest that the monolayer coverage of the adsorbed dyes at the outer surface of the adsorbent, this monolayer coverage increase with increasing temperature.

- Fitting the Freundlich model to the experimental data at different temperatures show that the adsorption of tested dyes on PAC is slightly higher

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than carbon soot and highly greater than granular carbon.

- Fitting the of Burnaur Emmett & Teller (BET) model to the experimental data at different temperatures show that the amount of dye adsorbed in forming a complete monolayer (Xm) on PAC is slightly higher than carbon soot and highly greater than granular carbon. It is found also that the amount of dye adsorbed in forming a complete monolayer (Xm) increase with increasing temperature.

NOMENCLATURE

- A: Constant describing the energy of interaction between the solute and the adsorbent surface
- a : Langmuir isotherm constant
- b : monolayer coverage constant
- C: Concentration of solute in solution at equilibrium (mg/l).
- Co: Initial dye concentration.
- C_s: Saturation concentration of solute (mg/l)
- K: adsorption capacity (Freundlich)
- m : Weight of adsorbent (mg)
- n : Freunlich adsorption constant
- RL: dimensionless seperation factor (Langmuir)
- x : Amount of solute adsorbed (mg)
- x/m: Amount of dye adsorbed per adsorbent
- X_m: Amount of solute adsorbed used in forming a complete monolayer, (mg/mg).
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Table 1: Analysis of Langmuir parameters of different dyes on different adsorbents at different temperatures.

(C) a b R ₁ R ² a b R ₂ R ² a b R ₃ R ² a b R ₄ R ² a b R ₄ R ² R ² B b R ₄ R ²	Dyc	Temp.		Granular can	r carbon	200		So	Soot			PAC	O.	
25 1.003 0.00990 0.00988 0.8660 63.31 0.0130 0.00091 0.893 59.83 0.0133 0.0001 40 2.322 0.0120 0.0042 0.962 74.14 0.0150 0.0004 0.962 74.14 0.0150 0.0004 0.0052 0.074 93.15 0.0100 0.975 57.58 0.0153 0.0001 0.095 68.44 0.0159 0.0001 0.095 68.44 0.0159 0.0001 0.095 68.44 0.0159 0.0001 0.095 68.44 0.0159 0.0001 0.095 68.44 0.0159 0.0001 0.095 68.44 0.0159 0.0001 0.095 68.44 0.0159 0.0001 0.095 68.44 0.0158 0.0001 0.095 68.44 0.0158 0.0001 0.095 6.0001 0.0002 0.0015 0.0001 0.0001 0.0015 0.0015 0.0001 0.0015 0.0015 0.0001 0.0015 0.0015 0.0001 0.0015 0.0015 0	1	(C)	u	þ	R	R²	S	Ď	R _t ,	. R ²	c	P	RL	R ²
40 2.322 0.0120 0.0042 0.962 74.14 0.0150 0.0001 0.973 57.58 0.0165 0.0001 50 3.049 0.0130 0.0032 0.974 93.15 0.0190 0.0000 0.855 68.44 0.0199 0.0001 4.965 0.0188 0.0020 0.950 112.26 0.0003 0.851 33.44 0.0159 0.0001 40 1.501 0.0074 0.0066 0.835 27.20 0.0125 0.0003 0.871 44.05 0.0159 50 1.501 0.0074 0.0066 0.885 36.36 0.0159 0.0003 0.871 0.0003 0.871 0.0003 0.871 0.0003 0.871 0.0003 0.872 0.0105 0.0003 0.872 0.0105 0.0003 0.873 0.0105 0.0003 0.873 3.475 0.0169 0.0001 40 1.636 0.0017 0.0067 0.056 0.272 0.0003 0.873 1.246	1	25	1.003	0.0000	0.0098	0.860	63.31	0.0130	0.0001	0.893	59.83	0.0133	0.0001	0.975
50 3.049 0.0130 0.0032 0.974 93.15 0.0190 0.0001 0.895 68.44 0.0199 0.0001 60 4.865 0.0188 0.0020 0.950 112.26 0.0210 0.0000 0.954 87.67 0.0121 0.0001 25 1.170 0.0076 0.0066 0.885 27.95 0.0139 0.0003 0.871 3.44 0.0158 0.0003 60 1.501 0.0076 0.0066 0.885 27.95 0.0103 0.0071 0.0060 0.886 6.685 0.0073 0.0240 0.913 24.13 0.0077 0.0003 0.893 18.40 0.0013 0.0014 0.0014 0.0024 0.0035 0.0003 0.004 0.0035 0.0003 0.0001 0.0014 0.0024 0.0035 0.0003 0.0003 0.0024 0.0035 0.0003 0.0003 0.0003 0.0003 0.0004 0.0035 0.0003 0.0004 0.0003 0.0003 0.0004 0.0003		40	2.322	0.0120	0.0042	0.962	74.14	0.0150	0.0001	0.973	57.58	0.0165	0.0001	0.911
60 4.965 0.0188 0.0020 0.950 112.26 0.0210 0.0000 0.954 87.67 0.0212 0.0000 25 1.175 0.0074 0.0084 0.929 28.32 0.0125 0.0003 0.881 33.44 0.0158 0.0003 40 1.501 0.0076 0.0066 0.882 27.93 0.0159 0.0003 0.873 44.05 0.0151 0.0002 50 1.536 0.0127 0.0069 0.886 36.36 0.0003 0.893 18.91 0.0013 0.0001 40 0.388 0.0090 0.0250 0.966 27.20 0.0095 0.0003 0.891 18.475 0.0169 0.0000 50 0.325 0.0156 0.0250 0.966 27.20 0.0095 0.0003 0.981 13.84 0.0004 0.998 154.75 0.0160 0.0001 50 0.528 0.0104 0.055 27.17 0.014 0.0003 0.924 154		20	3.049	0.0130	0.0032	0.974	93.15	0.0190	0.0001	0.895	68.44	0.0199	0.0001	0.885
25 1.173 0.0074 0.0084 0.929 28.32 0.0125 0.0003 0.881 33.44 0.0158 0.0002 40 1.501 0.0076 0.0066 0.885 27.93 0.0159 0.0003 0.873 44.05 0.0151 0.0002 50 1.346 0.0112 0.0073 0.866 3.536 0.0103 0.885 5.547 0.0169 0.0001 40 0.538 0.0073 0.0240 0.913 24.13 0.0007 0.0004 0.993 115.56 0.0078 0.0000 40 0.538 0.0097 0.0240 0.913 24.13 0.0004 0.993 115.56 0.0009 0.0009 50 0.525 0.030 0.959 27.12 0.0003 0.998 154.75 0.0169 0.0009 60 0.680 0.0359 27.02 0.0271 0.0003 0.998 154.75 0.0169 0.0009 50 0.687 0.011 0.0559	CH	09	4.965	0.0188	0.0020	0.950	112.26	0.0210	0.0000	0.954	87.67	0.0212	0.0001	0.791
40 1.501 0.0076 0.0056 0.835 27.95 0.0159 0.0003 0.875 44.05 0.0151 0.0002 50 1.346 0.0112 0.0073 0.951 31.44 0.0165 0.0003 0.893 35.47 0.0169 0.0001 50 1.346 0.0112 0.0073 0.0240 0.913 3.413 0.0102 0.893 38.91 0.0169 0.0001 40 0.388 0.0090 0.0240 0.994 2.413 0.0077 0.0004 0.993 11.5.56 0.0078 0.0001 50 0.325 0.0194 0.0240 0.959 3.018 0.0146 0.0003 0.981 15.475 0.0009 60 0.680 0.0104 0.959 27.02 0.0003 0.998 15.475 0.0169 0.0000 40 1.497 0.0110 0.0056 0.999 44.07 0.0271 0.0003 0.932 25.779 0.003 50 0.0150 <td>2</td> <td>25</td> <td>1.173</td> <td>0.0074</td> <td>0.0084</td> <td>0.929</td> <td>28.32</td> <td>0.0125</td> <td>0.0003</td> <td>0.881</td> <td>33.44</td> <td>0.0158</td> <td>0.0003</td> <td>0.935</td>	2	25	1.173	0.0074	0.0084	0.929	28.32	0.0125	0.0003	0.881	33.44	0.0158	0.0003	0.935
50 1.346 0.0112 0.0073 0.961 31.44 0.0163 0.0003 0.893 58.47 0.0169 0.00013 60 1.636 0.0127 0.0060 0.886 36.36 0.0198 0.0002 0.893 38.91 0.0001 25 0.394 0.0073 0.0240 0.913 24.13 0.0077 0.0004 0.993 115.56 0.0078 0.0000 40 0.388 0.0090 0.0250 0.966 27.20 0.0093 0.981 128.66 0.0099 0.0000 50 0.325 0.0136 0.0300 0.959 30.18 0.0146 0.0093 0.981 128.66 0.0099 0.0000 50 0.680 0.0144 0.0144 0.968 27.17 0.0151 0.0093 1.971 0.0003 0.954 15.77 0.0000 0.0094 0.0000 0.0094 0.0094 0.0098 0.0094 0.0094 0.0098 0.0094 0.0097 0.0099 0.0000		40	1.501	0.0076	0.0066	0.835	27.93	0.0139	0.0003	0.873	44.05	0.0151	0.0002	0.928
60 1.636 0.0127 0.0060 0.886 36.36 0.0198 0.0002 0.893 38.91 0.0020 0.0013 25 0.394 0.0073 0.0240 0.913 24.13 0.0077 0.0004 0.993 115.56 0.0078 0.0000 40 0.388 0.0090 0.0250 0.966 27.20 0.0095 0.991 128.66 0.0099 0.0000 50 0.325 0.0136 0.0300 0.959 30.18 0.0146 0.0009 0.998 154.75 0.0160 0.0000 60 0.680 0.0144 0.968 27.17 0.0146 0.0009 0.998 154.75 0.0160 0.0000 40 1.497 0.0110 0.0066 0.999 44.07 0.0301 0.0927 3.51.42 0.0157 0.0000 50 0.0150 0.0191 0.872 27.71 0.0302 0.972 27.72 0.0302 0.972 27.72 0.0302 0.972 <td< td=""><td></td><td>50</td><td>1.346</td><td>0.0112</td><td>0.0073</td><td>0.961</td><td>31.44</td><td>0.0163</td><td>0.0003</td><td>0.895</td><td>55.47</td><td>0.0169</td><td>0.0001</td><td>0.947</td></td<>		50	1.346	0.0112	0.0073	0.961	31.44	0.0163	0.0003	0.895	55.47	0.0169	0.0001	0.947
25 0.394 0.0073 0.0240 0.913 24.13 0.0077 0.0004 0.995 115.56 0.0078 0.0000 40 0.388 0.0090 0.0250 0.966 27.20 0.0095 0.0003 0.981 128.66 0.0099 0.0000 50 0.325 0.0136 0.0300 0.959 50.18 0.0146 0.0009 128.66 0.0099 0.0000 25 2.473 0.0134 0.0144 0.0144 0.0159 27.02 0.0271 0.0003 0.928 154.75 0.0160 0.0000 25 2.473 0.00097 0.0040 0.959 27.02 0.0271 0.0003 0.928 121.61 0.0157 0.0000 40 1.497 0.0110 0.0056 0.999 44.07 0.0309 0.0002 0.972 151.61 0.0157 0.0000 50 0.515 0.0150 0.0059 0.0057 0.0572 152.72 0.0372 10211 0.0000	H	09	1.636	0.0127	0.0060	0.886	36.36	0.0198	0.0002	0.893	38.91	0.0201	0,0013	0.841
40 0.388 0.0090 0.0250 0.966 27.20 0.0095 0.0003 0.981 128.66 0.0099 0.0000 50 0.325 0.0136 0.0300 0.959 30.18 0.0146 0.0003 0.998 154.75 0.0160 0.0000 60 0.680 0.0134 0.0144 0.968 27.17 0.0151 0.0003 0.938 154.75 0.0160 0.0000 25 2.473 0.0097 0.0040 0.959 27.02 0.0271 0.0003 0.924 295.79 0.0000 40 1.497 0.0110 0.0066 0.999 44.07 0.0301 0.0002 0.972 315.92 0.0337 0.0000 50 0.872 0.0150 0.0113 0.974 37.82 0.0309 0.0002 0.972 311.42 0.0376 0.0000 50 0.0057 0.0190 0.024 37.82 0.0309 0.0004 0.995 236.74 0.0191 0.0001 <td>'n</td> <td>25</td> <td>0.394</td> <td>0.0073</td> <td>0.0240</td> <td>0.913</td> <td>24.13</td> <td>0.0077</td> <td>0.0004</td> <td>0.993</td> <td>115.56</td> <td>0.0078</td> <td>0.0000</td> <td>0.774</td>	'n	25	0.394	0.0073	0.0240	0.913	24.13	0.0077	0.0004	0.993	115.56	0.0078	0.0000	0.774
50 0.325 0.0136 0.0300 0.959 30.18 0.0146 0.0003 0.998 154.75 0.0160 0.0000 60 0.680 0.0144 0.968 27.17 0.0151 0.0003 0.924 295.79 0.0000 25 2.473 0.0097 0.0040 0.959 27.02 0.0271 0.0003 0.924 295.79 0.0298 0.0000 40 1.497 0.0110 0.0066 0.999 44.07 0.0301 0.0002 0.972 295.79 0.0298 0.0000 50 0.515 0.0150 0.0113 0.974 37.82 0.0309 0.0002 0.673 371.42 0.0337 0.0000 50 0.0150 0.0111 0.837 22.71 0.0430 0.0004 0.852 92.99 0.0153 0.0001 0.996 237.12 0.0191 0.0001 40 1.116 0.0141 0.0088 0.852 92.99 0.0151 0.0009 0.996 <t< td=""><td></td><td>40</td><td>0.388</td><td>0.0000</td><td>0.0250</td><td>0.966</td><td>27.20</td><td>0.0005</td><td>0.0003</td><td>0.981</td><td>128.66</td><td>0.0099</td><td>0.0000</td><td>0.941</td></t<>		40	0.388	0.0000	0.0250	0.966	27.20	0.0005	0.0003	0.981	128.66	0.0099	0.0000	0.941
60 0.680 0.0144 0.0468 27.17 0.0151 0.0003 0.938 121.61 0.0157 0.0000 25 2.473 0.0097 0.0040 0.959 27.02 0.0271 0.0003 0.924 295.79 0.0298 0.0000 40 1.497 0.0110 0.0056 0.999 44.07 0.0301 0.0002 0.972 215.92 0.0298 0.0000 50 0.872 0.0150 0.0113 0.974 37.82 0.0309 0.0673 371.42 0.0376 0.0000 60 0.515 0.0190 0.0151 0.0430 0.0004 0.822 1021.1 0.0472 0.0000 25 1.005 0.0097 0.0098 0.724 85.34 0.0151 0.0001 0.995 236.74 0.0191 0.0001 40 1.116 0.0141 0.0088 0.852 92.99 0.0151 0.0001 0.996 237.12 0.0211 0.0001 60 0.		20	0.325	0.0136	0.0300	0.959	30.18	0.0146	0.0003	0.998	154.75	0.0160	0.0000	0.910
25 2.473 0.0097 0.0040 0.959 27.02 0.0271 0.0003 0.924 295.79 0.0298 0.0000 40 1.497 0.0110 0.0066 0.999 44.07 0.0301 0.0002 0.972 315.92 0.0337 0.0000 50 0.872 0.0150 0.0113 0.974 37.82 0.0309 0.0002 0.673 371.42 0.0376 0.0000 60 0.513 0.0191 0.837 22.71 0.0430 0.0004 0.872 1021.1 0.0472 0.0000 25 1.005 0.0097 0.0098 0.724 85.34 0.0155 0.0001 0.995 236.74 0.0191 0.0001 40 1.116 0.0111 0.0088 0.852 92.99 0.0151 0.0000 0.996 237.12 0.0211 0.001 50 1.211 0.0141 0.0065 0.965 79.60 0.0251 0.0001 0.900 298.08 0.0331 <t< td=""><td></td><td>09</td><td>0.680</td><td>0.0144</td><td>0.0144</td><td>0.968</td><td>27.17</td><td>0.0151</td><td>0.0003</td><td>0.938</td><td>121.61</td><td>0.0157</td><td>0.0000</td><td>0.995</td></t<>		09	0.680	0.0144	0.0144	0.968	27.17	0.0151	0.0003	0.938	121.61	0.0157	0.0000	0.995
40 1.497 0.0110 0.0056 0.999 44.07 0.0301 0.0002 0.972 515.92 0.0337 0.0000 50 0.872 0.0150 0.0113 0.974 37.82 0.0309 0.0002 0.673 371.42 0.0376 0.0000 60 0.513 0.0190 0.837 22.71 0.0430 0.0004 0.822 1021.1 0.0472 0.0000 25 1.005 0.0097 0.0098 0.724 85.34 0.0135 0.0001 0.995 236.74 0.0191 0.0001 40 1.116 0.0111 0.0088 0.852 92.99 0.0151 0.0001 0.996 237.12 0.0191 0.0001 50 1.211 0.0141 0.0081 0.944 172.07 0.0161 0.0000 298.08 0.0331 0.0001 60 0.554 0.0165 0.965 79.60 0.0001 0.9900 298.08 0.0331 0.0001	ব	25	2.473	0.0097	0.0040	0.959	27.02	0.0271	0.0003	0.924	295.79	0.0298	0.0000	0.995
50 0.872 0.0150 0.0113 0.974 37.82 0.0309 0.0002 0.673 371.42 0.0376 0.0000 60 0.513 0.0190 0.0837 22.71 0.0430 0.0004 0.822 1021.1 0.0472 0.0000 25 1.005 0.0097 0.0098 0.724 85.34 0.0135 0.0001 0.995 236.74 0.0191 0.0001 40 1.116 0.0111 0.0038 0.852 92.99 0.0151 0.0001 0.996 237.12 0.0191 0.0001 50 1.211 0.0141 0.0081 0.944 172.07 0.0161 0.0000 0.989 275.31 0.0233 0.0001 60 0.554 0.0165 0.965 79.60 0.0251 0.0001 0.900 298.08 0.0331 0.0001		40	1.497	0.0110	0.0066	0.999	44.07	0.0301	0.0002	0.972	315.92	0.0337	0.0000	0.708
60 0.515 0.0190 0.0191 0.837 22.71 0.0430 0.0004 0.822 1021.1 0.0472 0.0000 25 1.005 0.0097 0.0098 0.724 85.34 0.0135 0.0001 0.995 236.74 0.0191 0.0001 40 1.116 0.0111 0.0088 0.852 92.99 0.0151 0.0001 0.996 237.12 0.0191 0.0001 50 1.211 0.0141 0.0081 0.944 172.07 0.0161 0.0000 0.989 275.31 0.0233 0.0001 60 0.554 0.0165 0.965 79.60 0.0251 0.0001 0.900 298.08 0.0331 0.0001		50	0.872	0.0150	0.0113	0.974	37.82	0.0309	0.0002	0.673	371.42	0.0376	0.0000	0.790
25 1.005 0.0097 0.0098 0.724 85.34 0.0135 0.0001 0.995 236.74 0.0191 0.0001 40 1.116 0.0111 0.0088 0.852 92.99 0.0151 0.0001 0.996 237.12 0.0211 0.0001 50 1.211 0.0141 0.0081 0.944 172.07 0.0161 0.0000 0.989 275.31 0.0233 0.0001 60 0.354 0.0254 0.0165 0.965 79.60 0.0251 0.0001 0.900 298.08 0.0331 0.0001	Ä	09	0.513	0.0190	0.0191	0.837	22.71	0.0430	0.0004	0.822	1021.1	0.0472	0.0000	0.782
40 1.116 0.0111 0.0038 0.852 92.99 0.0151 0.0001 0.996 237.12 0.0211 0.0001 50 1.211 0.0141 0.0081 0.944 172.07 0.0161 0.0000 0.989 275.31 0.0233 0.0001 60 0.554 0.0254 0.0165 0.965 79.60 0.0251 0.0001 0.900 298.08 0.0331 0.0001	מי	25	1.005	0.0097	0.0098	0.724	85.34	0.0135	0.0001	0.995	236.74	0.0191	0.0001	0.826
50 1.211 0.0141 0.0081 0.944 172.07 0.0161 0.0000 0.989 275.31 0.0233 0.0001 60 0.554 0.0254 0.0165 0.965 79.60 0.0251 0.0001 0.900 298.08 0.0331 0.0001		40	1.116	0.0111	0.0088	0.852	92.99	0.0151	0.0001	966.0	237.12	0.0211	0.0001	0.725
60 0.554 0.0254 0.0165 0.965 79.60 0.0251 0.0001 0.900 298.08 0.0331 0.0001		50	1.211	0.0141	0.0081	0.944	172.07	0.0161	0.0000	0.989	275.31	0.0233	0.0001	0.645
Triedul S. Johnson, M. 19872-18 (P. Visco, M. Visco, M. II. V		(19	0.594	0.0254	0.0165	0.965	09.62	0.0251	0.0001	0.900	298.08	0.0331	0.0001	0.648
Tuestii Tuestii 17 Saatte M Pree (1 (1491) 11 Al-Sara Ventii				A A	CB CB	Dia beni	turit mid 88	NA NA NA	21	outs C. F	wis			AT
ubuti Ciqq Ciqq mine2 [Vi oo; V (Vi) Al 2 (v) ioo;					il a		bett		TS VE		4	100	7 1	200
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TO THE STATE OF TH			Sea Pa		4	FA FA	il A		M		H A	3		Sel
										91	50	11	10	K

Table 2 : Analysis of Freundlich parameters of different dyes on different adsorbents at different temperatures.

	emp.	5	Granular carbon	uo.		Soot			PAC	
		r,	×	R ²	u	×	R²	ជ	×	. K
	25	1.492	1.21	0.621	1.891	1.616	0.994	2.016	1.49	0.84
	40	1.193	1.29	0.735	1.986	2.099	0.983	2.574	1.43	0.98
	20	1.772	1.372	0.863	2.45	3.526	0.991	2.47	2.53	0.96
	99	1.811	1.451	0.998	2.266	5.013	0.976	2.602	4.207	0.95
7	25	1.482	1.015	0.697	2.125	1.164	0.811	2.101	1.235	0.926
	40	1.312	1.018	0.738	1.926	1.26	0.948	2.330	1.343	0.86
	20	1.792	1.041	0.819	1.981	1.32	0.831	1.996	1.39	0.83
	09	1.826	1.142	0.972	2.214	1.384	0.993	2.391	1.495	0.95
m	25	1.748	1.501	0.765	1.295	1.287	0.745	3.074	2.114	0.94
	40	1.111	1.581	0.701	1.508	1.581	0.970	2.381	2.205	0.87
	50	1.169	2.137	0.681	1.861	1.588	0.993	3.037	2.285	0.89
	09	1.971	1.651	0.756	2.491	1.738	0.979	4.859	2.55	0.95
4	25	1.191	8.729	0.528	1.353	1.774	0.756	1.783	2.317	0.69
	40	1.012	1.206	0.726	1.233	1.794	0.811	1.707	3.045	0.65
	50	1.383	1.384	0.807	1.335	2.843	0.891	1.778	3.713	0.84
	09	1.462	1.686	0.928	1.339	4.599	0.842	1.989	5.843	0.84
5	25	1.201	2.331	0.562	1.196	1.23	0.889	2.184	1.699	0.89
	40	1.339	2.603	0.654	1.233	1.87	0.959	2.196	2.137	0.70
	20	1.111	3.306	0.753	1.335	2.744	0.979	2.207	2.71	0.96
	09	1.456	4.018	0.820	1.632	4.639	0.960	2.146	3.398	0.95

Table 3: Analysis of BET parameters of different dyes on different adsorbents at different temperature.

Dye	Temp.	Ö	emulei carbo	띪		Soot			PAC	
	(၃	٧	 	R ²	Y	×	R²	¥	×	
-	25	0.0083	1.195	0.914	0.052	2.433	0.66.0	0.125	2.853	0.945
	40	0,0048	1.606	0.954	0.0129	3.87	0.999	0.077	3.307	0.990
	50	0,0017	2.839	0.884	0.0175	4.632	0.994	0.076	4.809	0.896
	09	0.0016	3.314	0.987	0.00716	4.879	0.963	0.032	5.365	0.994
2	2.5	0.0027	3.239	0.974	0.0304	5.809	0.867	0.853	8.603	0.935
	40	0.002	2.58	0.978	0.007	5.948	0.869	0.021	7.12	0.983
	50	0.0019	4.454	0.903	0.019	7.353	0.835	0.0139	8.588	0.943
	09	0.0013	5.316	0.968	0.0098	8.24	0.938	0.0341	8.987	0.823
m	25	0.00073	4.694	0.974	0.00023	6.39	0.984	0.0002	7.705	0.923
	40	0.00006	5.034	0.978	0.000%	6.12	0.993	0.00043	7.866	0.786
	20	0.00005	6.406	0.992	0.00015	8.11	0.941	0.00081	5.16	0.66.0
	09	0.0006	6.375	0.979	0.00081	8.60	0.984	0.0032	8.587	0.991
4	25	0.0161	1.436	0.952	0.256	3.993	0.918	0.302	4,845	0.992
	40	0.00549	1.773	196.0	0.105	3,1033	0.924	0.0405	4.988	0.946
	20	0.0057	3,195	0.993	96+0.0	4.518	0.857	0.0275	6.047	0.912
	09	0.0032	4.48	0.993	0.0239	5.919	0.976	0.0205	6.669	0.915
	25	0.158	1.002	0.994	0.271	1.849	0.995	0.298	1.87	0.660
2	40	0.0765	1.78	0.885	0.1053	3.104	966.0	0.0405	3.995	0.991
	50	0.0632	2.005	0.949	0.0496	4.5188	0.999	0.0275	5.050	0.996
	09	0.051	2.6317	0.965	0.0152	5.189	666.0	0.0205	6.999	0.998