DESIGN OF A ROBUST ELECTRO-MECHANICAL CONTROL SYSTEM

عدوان البحث :- تصميم لانون تحكم لمنظومة كهروميكانيكية

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ملكم البحدي-

يلام البحدث طريلة ملترجبة لتصميم دظام شحاكم لمنظومة كبروميكانيكية، و يعتاوى البحث على النموذج الرياضي لمنظومة كبروميكانيكية مكونة من محرك شيار مستمر محكوم من داخرة العلم السدوار و مولد شيار مخردد ذو وجه واعد. و هذه المنظومة لها غرجان يتم التحكم ليهما و هما الشردد و اللدرة الناشخشين من المولد ذو الشيار المشردد و ذلك حتى يمكن غبطهما لشغلية محرك شيار مدردد للتحكم في سرعته.

و المحتظومة المذكورة متظومـة غير غطية ولذلك عم استعتاج لاانون المتحكم لهذه المنظومة بأستحدام طريلة البذك اللاغطى.

وقد بينت المحاكاة والنتائج لهمالية الطريقة المقترحة في تصميم نظام التعشم للمنظومة الكهروميكانيكية.

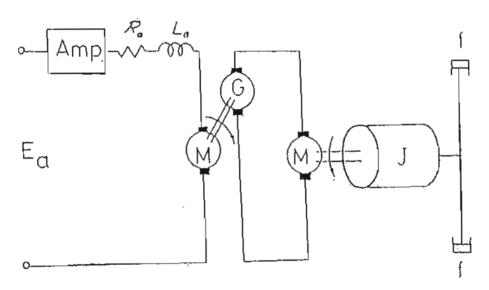
ABSTRACT:

The paper introduces a suggested technique for the design of a nonlinear electromechanical control system. The suggested design is applied to a motor-generator set. This technique electromechanical system is nonlinear and at the same multivariable. The effect of a nonlinear power amplifier included in the system is also considered. The main objective of such design is to generate electrical power with low harmonic content, which is necessary for the speed control of a.c. motors. The motor-generator set represents a multivariable system since, it required to control both the frequency and amplitude of the power. The system has also two inputs, the voltage at the terminals and the excitation voltage of the general affects both outputs and hence, decoupling is require multivariable system. The system is nonlinear by i' hence, a nonlinear approach is used for the design controller. Therefore, the suggested design tech the nonlinear cancellation approach. The pe nonlinear mathematical model of the electro the state space form. A numerical exaillustrate the effectiveness of the desir suggested design technique. Simulation of the electromechanical system v external disturbance on the load s

INTRODUCTION:

Electromechanical systems are usually exposed to different types of nonlinearities, which affect severely the dynamic performance of such systems. The electro-mechanical system shown in fig. (1) consists of a single phase alternator, driven by an armature controlled d. c. motor. The objective of this work is to design a nonlinear compensator for controlling the frequency and the amplitude of the a.c. power at the output terminals of the single phase alternator. The shown motor-generator set has two inputs, these inputs are the motor armature voltage and the field voltage of the alternator.

MATHEMATICAL MODEL OF THE SYSTEM: the mathematical model of the system can be represented in state space (1), by the following set of differential equations:



Flg. (1)

$$x_{1} = -\frac{R_{L}}{L} \quad x_{1} + \frac{K_{g}}{L} \quad x_{g} \quad x_{2}$$
 (1)

$$x_{2} = \frac{Fg}{J_{g}} x_{z} + \frac{1}{J_{g}} x_{s} - \frac{Kg}{J_{g}} x_{s} x_{s}$$
(2)

$$= K_{g}(x_{4} - x_{2}) \tag{3}$$

$$\dot{x}_{4} = \frac{F_{m}}{J_{m}} \times_{4} - \frac{1}{J_{m}} \times_{9} + \frac{K_{m}}{J_{m}} \times_{5} \tag{4}$$

$$x_{s} = -\frac{r_{f}}{L} x_{s} + \frac{1}{L} u_{g}$$
 (6)

$$v_{A} = R_{L} \times_{A} \tag{7}$$

$$z = x_{\perp}$$
 (8)

where:

x, = load current,

 $x_{a} = angular velocity of the generator,$

 x_{a} = the torque available to drive the generator,

 $x_i = angular velocity of the motor.$

 $x_{\perp} = armature current of the motor,$

 $x_s =$ field current of the generator.

K = shaft stiffness, $r_{\alpha}^{s}, L_{\alpha} = motor armature resistance and inductance respectively.$

 R_{L} , L = local resistance and inductance respectively.

r, L, = generator field resistance and inductance respectively.

r L friction coefficient and rotor inertia = viscous respectively,

 $F_{q}, J_{q} = viscous$ friction coefficient of the generator itsinertia,

 F_{m} , J_{m} = viscous friction coefficient of the motor and load

 K_{a}, K_{m} = generator and motor torque constants respectively,

= input armature voltage to the motor,

= input field voltage to the alternator.

= load voltage,

= angular velocity of the generator,

Compensator design via nonlinear cancellation:

The model represented by equations (1) \rightarrow (8) can be re-written in the input/output form as follows [2,4] using equations (2), (7) & (8) we can write:

$$y_2 = -\frac{k_m^2}{Jr_a} y_2 - \frac{1}{JR_L} \frac{y_1^2}{y_2} + \frac{k_m}{Jr_a} u_s$$
 multiplying both sides by y_2 we get

$$y_{2}y_{2} = \frac{k_{m}^{2}}{Jr} y_{2}^{2} - \frac{1}{JR} y_{1}^{2} + \frac{k_{m}}{Jr} y_{2}u_{1}$$
 (9)

Also, from (7) we have